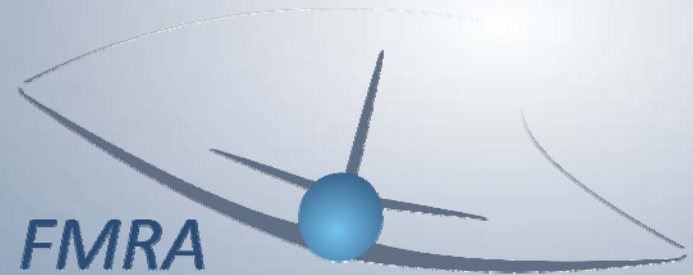


FMRA

Fachgebiet Flugmechanik, Flugregelung und Aeroelastizität

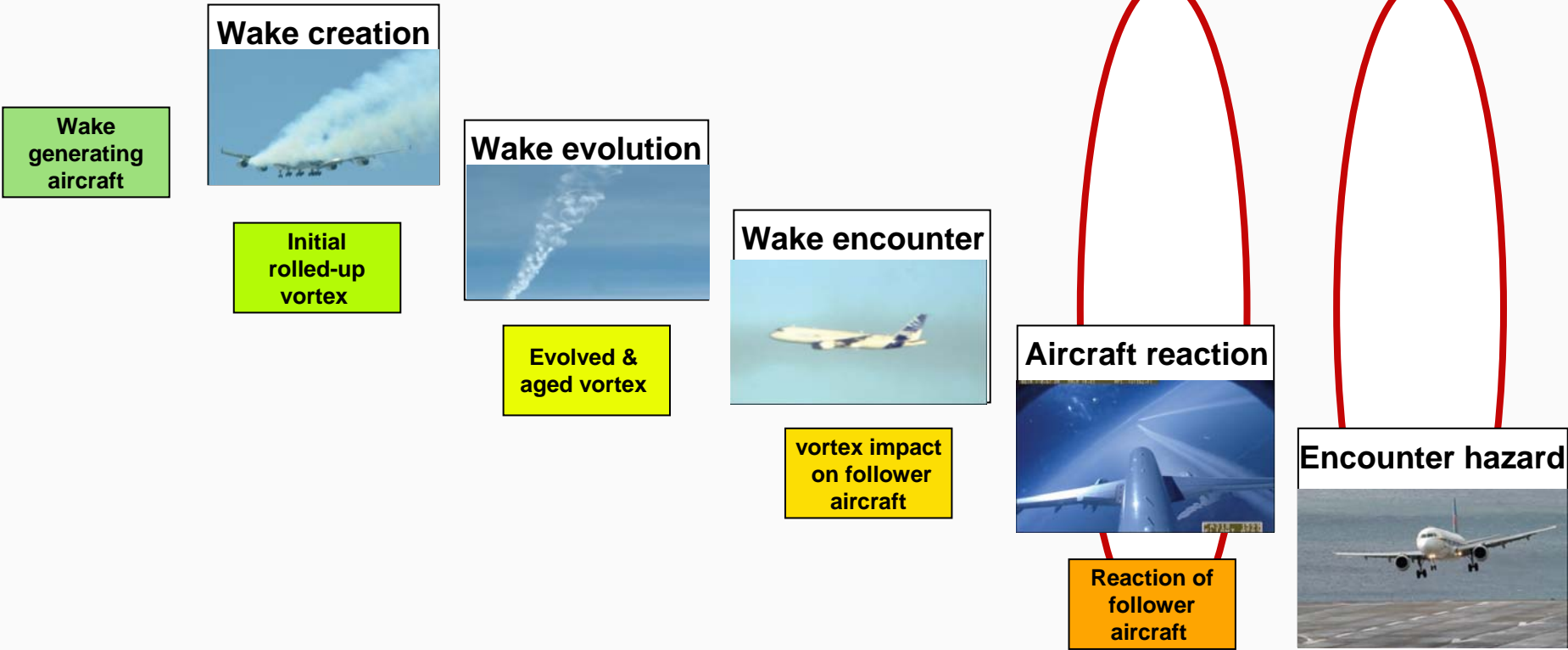


Overview on pilot models for wake vortex encounter simulations

- Robert Luckner



**Day 2
Models of Pilot Behaviour
and Severity Assessment**



The models are needed for safety and risk assessments of new separation standards

Source: Airbus

Pilot models for wake vortex encounter risk assessment

Pilot behavioural models

- for manual flight
- for automatic flight (autopilot / auto throttle)

Severity criteria that represent pilots perception of a WVE

Objectives and expected outcome of day 2:

- 1) Summary of existing, state-of-the-art pilot models for
 - a) pilot control behaviour
 - b) severity assessment (severity criteria)

- 2) Evaluation of these state-of-the-art models and identification of research needs

- 3) Contribution to the WakeNet3-Europe report on Research Needs
regarding “Wake vortex models for encounter simulations in real-time piloted simulator tests and for fast-time flight simulations for risk assessment”.

National Research Council (NRC), US:

Wake Turbulence - An Obstacle to Increased Air Traffic Capacity, pp 48 (2008)

On “Safety Analysis and Hazard Boundaries”:

- **Finding**

- 3.14 Although the current air transportation system was designed to avoid wake vortex encounters, they do occur and are safely tolerated using present spacing criteria

- 3.15 It is difficult to quantify acceptable reductions in wake turbulence spacing because there is no agreed metric for, nor definition of, hazard boundaries for wake encounters

- **Recommendation**

- regarding pilot control behavior models: none

- 3.11 A **hazard boundary** needs to be defined and used as a metric in forming spacing criteria

National Research Council (NRC), US:

Wake Turbulence - An Obstacle to Increased Air Traffic Capacity (2008)

- **Milestones for Wake Vortex Modeling**

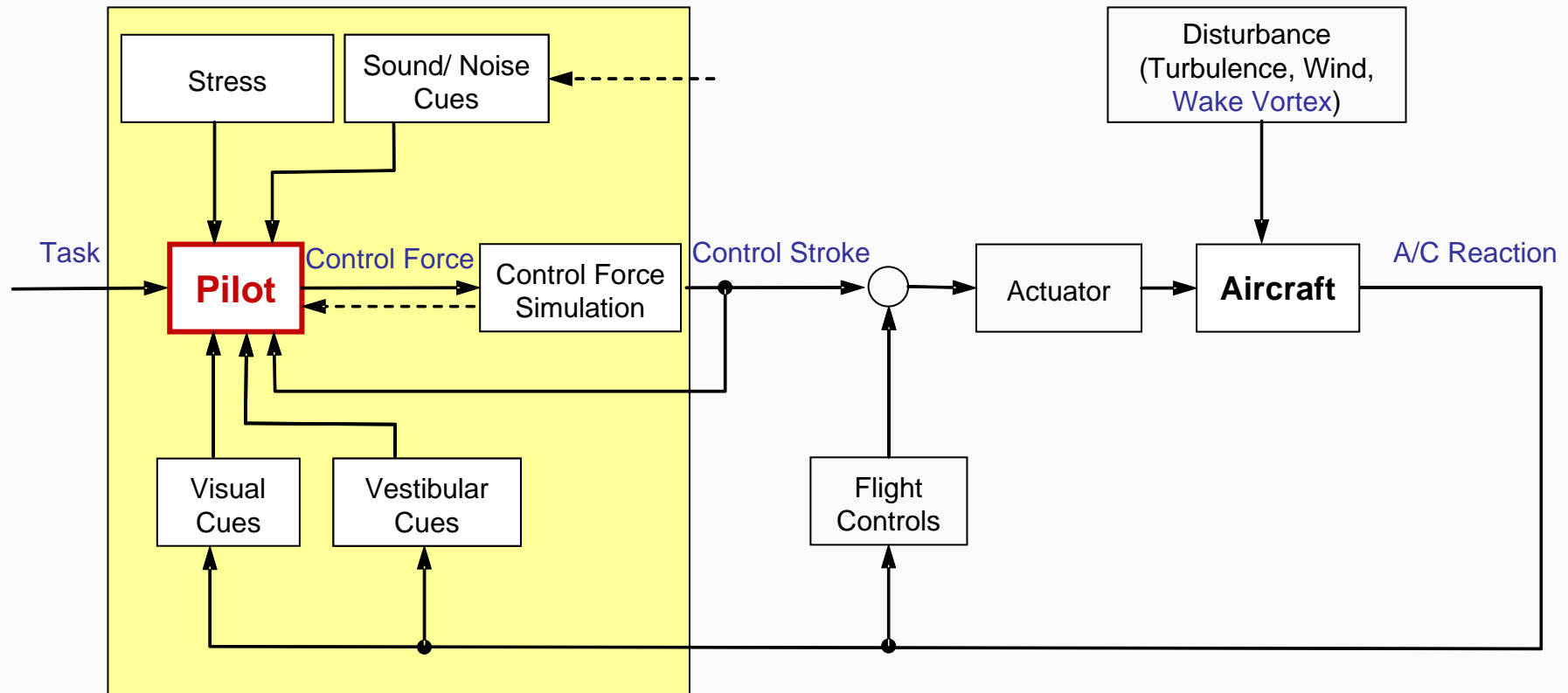
Time Horizon	Milestone
1) Short term	<ul style="list-style-type: none"> a) Identify metrics for hazard definition b) Review European studies and complete detailed plan for simulator studies c) Begin conducting simulator studies d) Identify conservative hazard boundaries
2) Medium term	<ul style="list-style-type: none"> a) Analyse results from simulator studies to quantify hazard b) Develop risk assessment methodology and apply it to simulator studies c) Refine hazard boundaries based on available data
3) Long term	<ul style="list-style-type: none"> a) Test and implement refined hazard boundary b) Demonstrate real-time safety analysis in actual flight

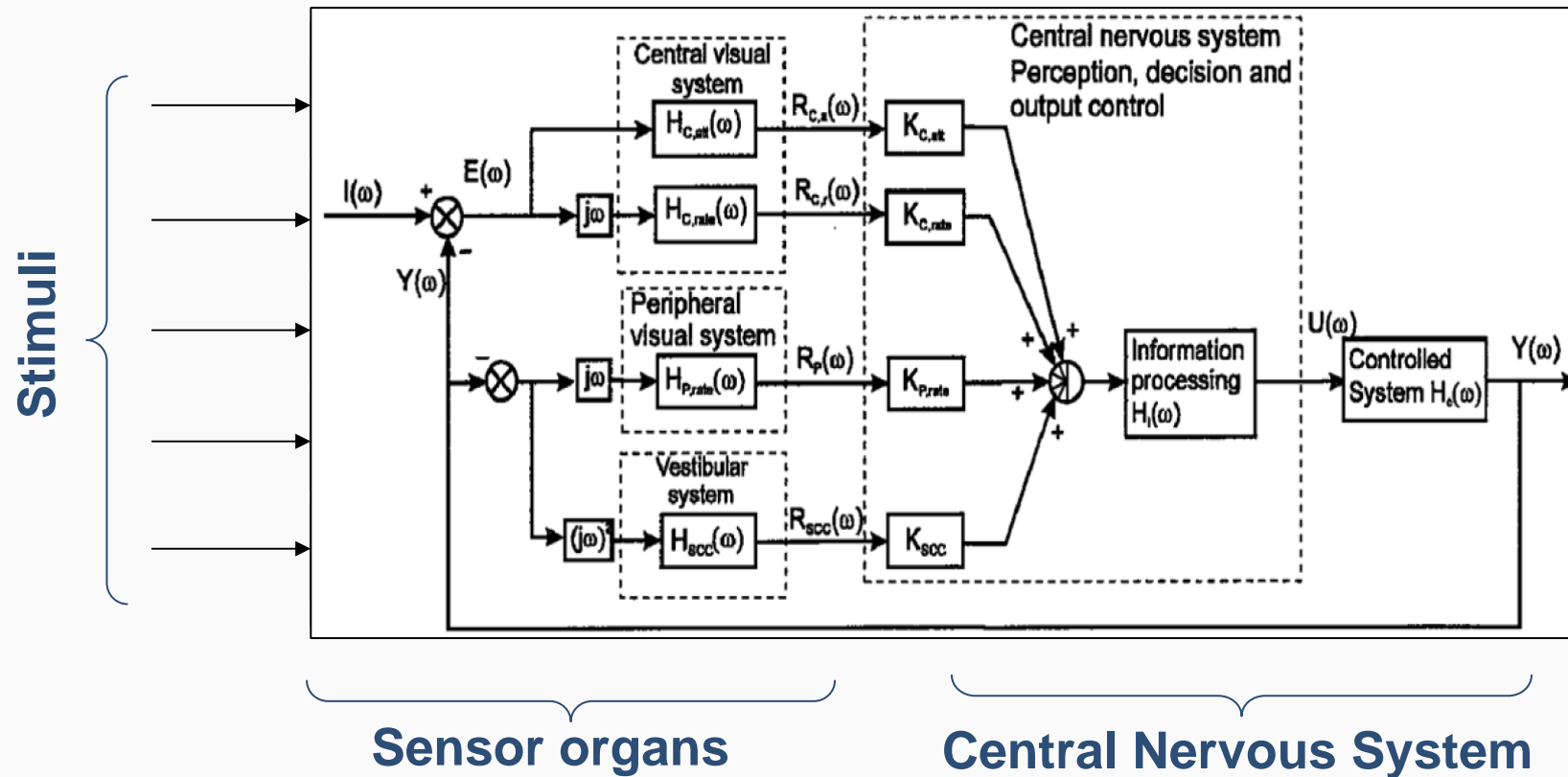
WakeNet2-Europe in Collaboration with WakeNet-USA: Wake Vortex Research Needs for Improved Wake Vortex Separation Ruling and Reduced Vortex Signatures (March 2006)

- **Recommendation (Part 2, pp 49)**

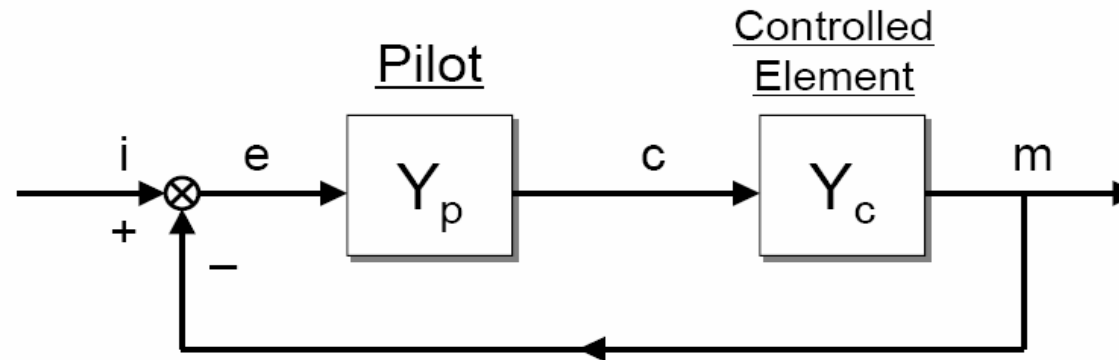
Reliable definitions of (non-)**hazard criteria** (levels) are urgently required, ...

For offline severity assessment of manually controlled flights wake vortex encounter **pilot models** are necessary and have been developed for the approach situation in S-WAKE. But for other flight phases, like departure, models are lacking. ...





Quelle: S. Advani



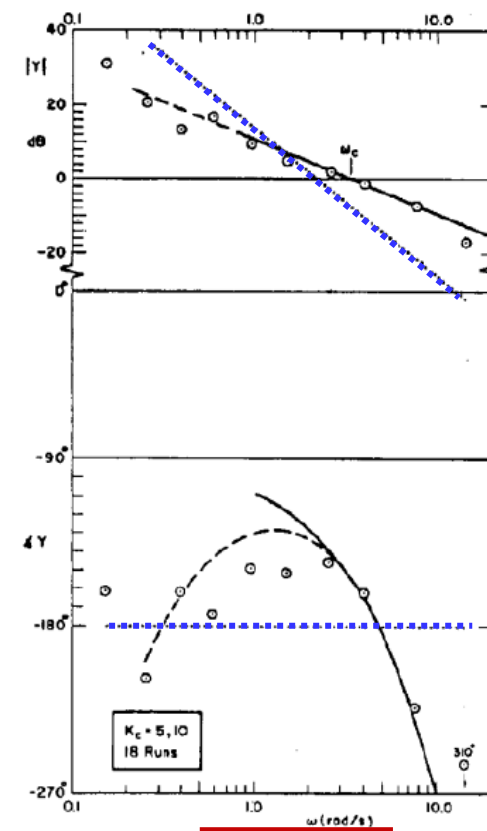
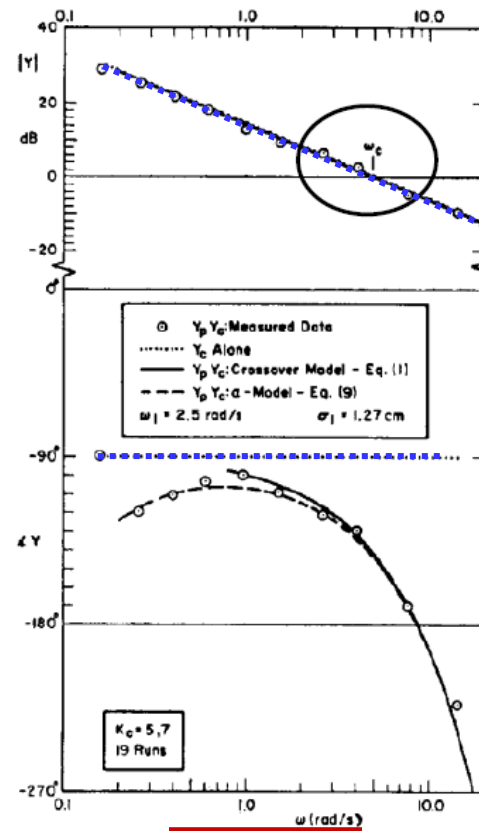
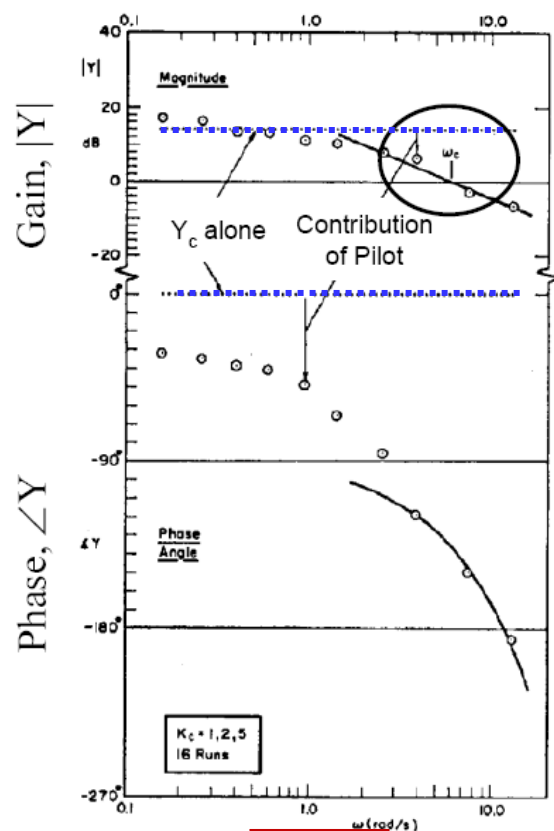
- ▶ Pilot adopts sufficient lead or lag so that the open-loop transfer function becomes :

$$Y_{OL}(j\omega) = Y_p Y_c \cong \frac{\omega_c e^{-j\omega\tau_e}}{j\omega}$$

near ω_c , i.e., the crossover frequency. (τ_e = effective time delay)

■ Crossover Models for $Y_C = K$, K/s , and K/s^2

- ▶ The open-loop transfer function ($Y_{OL} = Y_C Y_P$) has slope of approx. -20 dB/decade (solid line) in the crossover-frequency (ω_c) region.

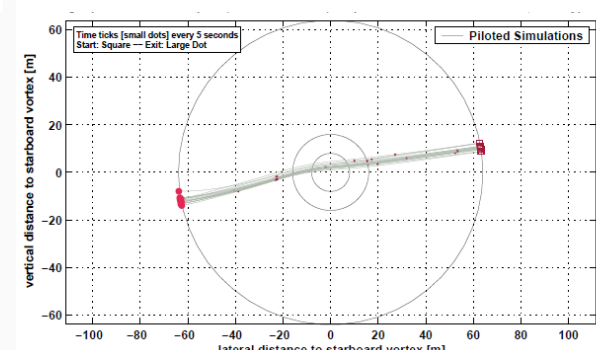
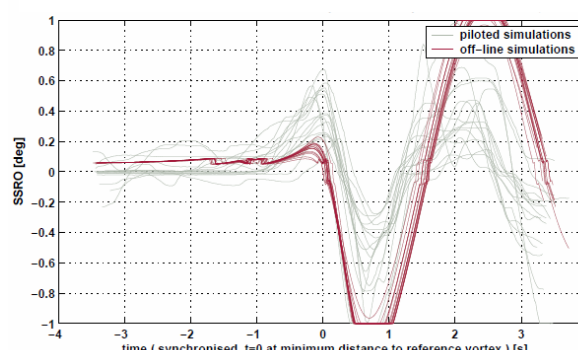
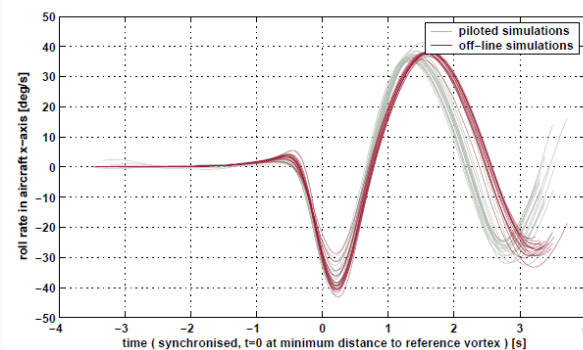
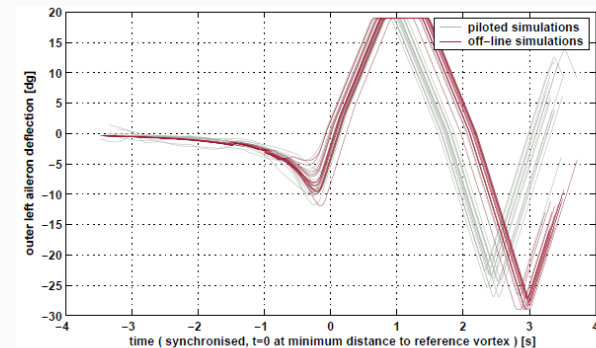
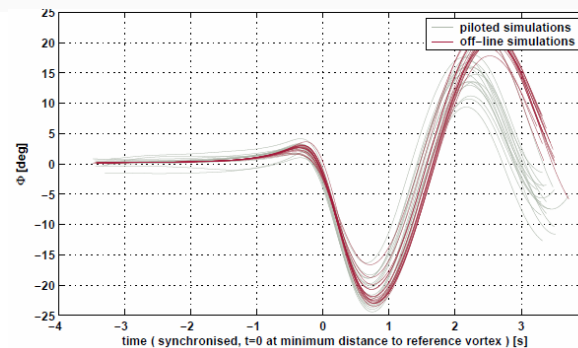
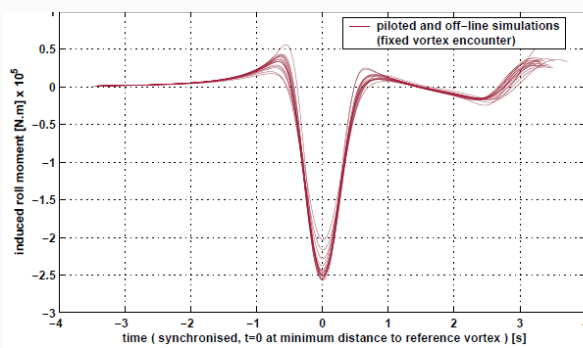


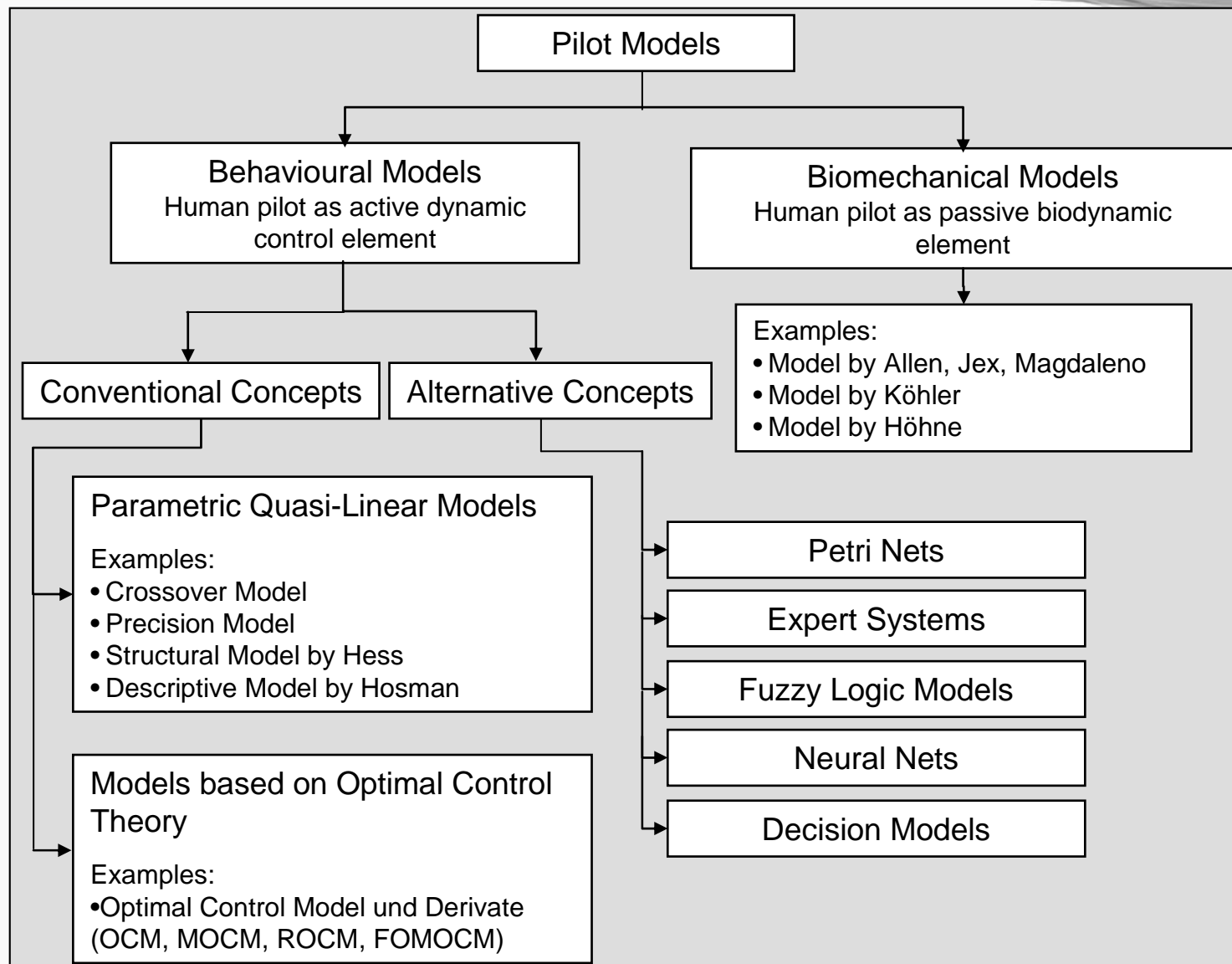
Controlled Element: $Y_c(s)$	Related Aircraft Control Situations	Pilot's Describing Function
K_c		$K_p e^{-j\omega\tau_e} / (T_I j\omega + 1)$
K_c / s		$K_p e^{-j\omega\tau_e}$
K_c / s^2		$K_p (T_L j\omega + 1) e^{-j\omega\tau_e}$
$K_c / s(Ts + 1)$	Roll angle control by ailerons.	If $T > \tau_e$, $K_p (T_L j\omega + 1) e^{-j\omega\tau_e}$ If $T < \tau_e$, $K_p e^{-j\omega\tau_e}$

Crossover Pilot Model

$$K_p \frac{1 + \tau_{\text{lead}}s}{1 + \tau_{\text{lag}}s} e^{-T_p s}$$

Pilot-Aircraft response in a wake vortex encounter:





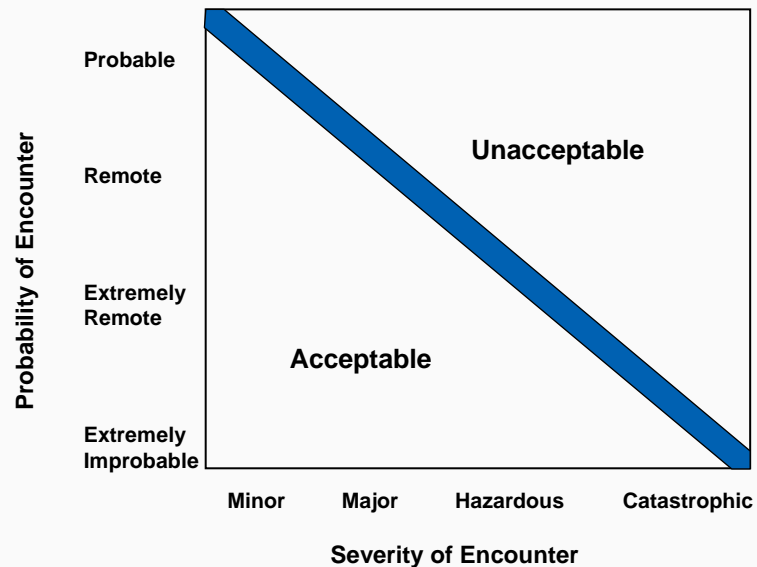
Severity Criteria

- **Metrics**

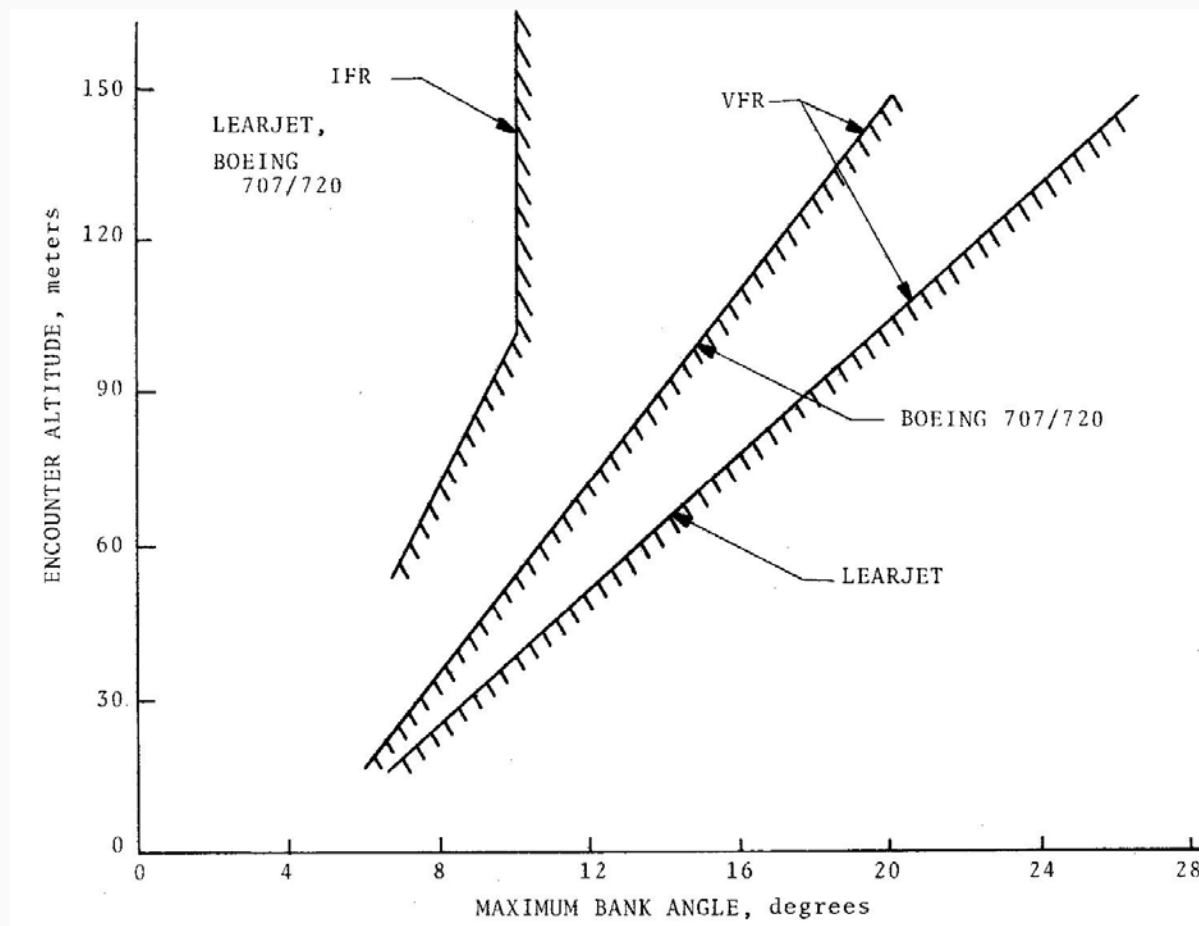
bank angle, roll rate, roll acceleration, roll control ratio (RCR)
as a function of height above ground

- **Boundaries**

What is acceptable?
different levels?
levels depending on probability



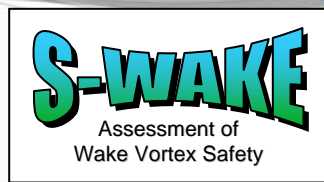
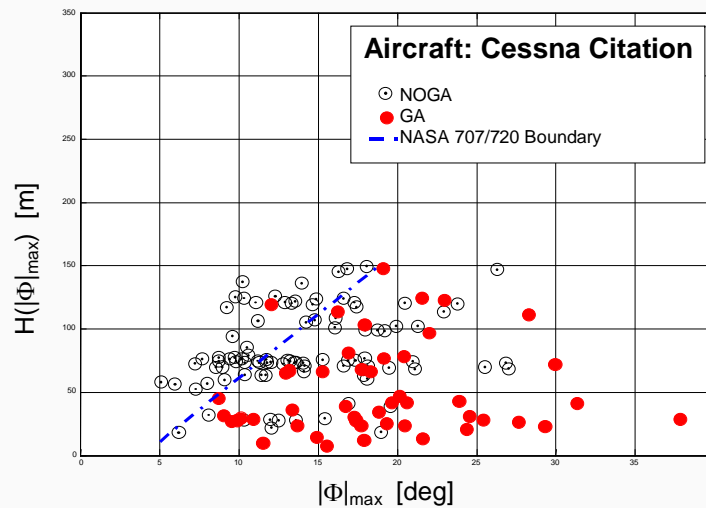
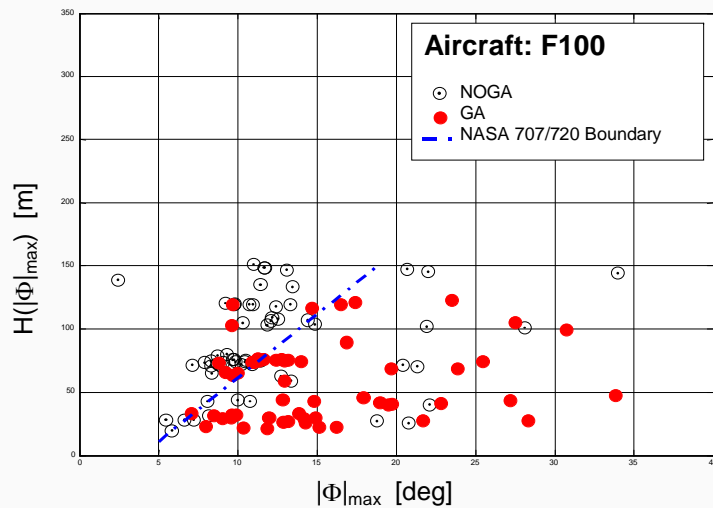
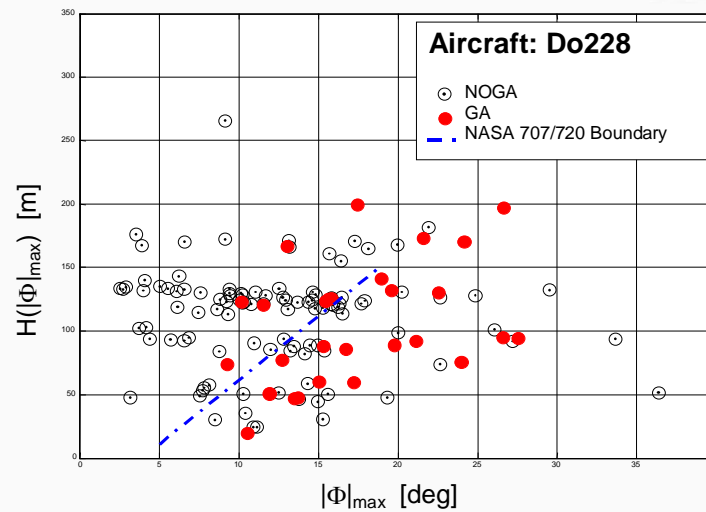
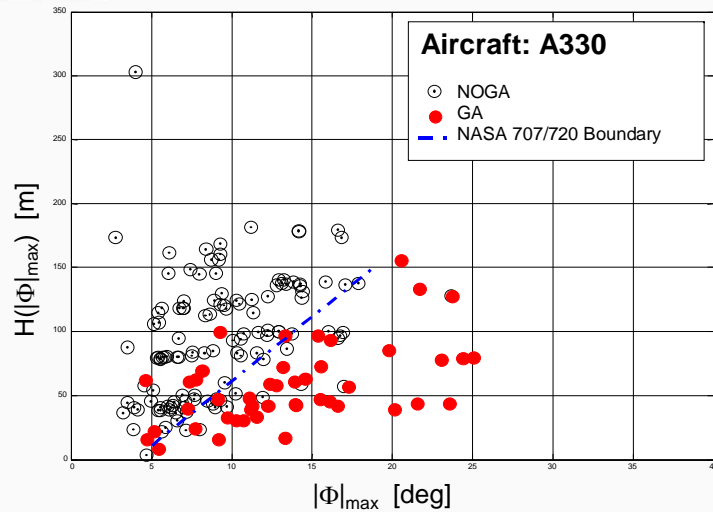
Results of NASA simulation experiments



Sammonds R.I., Stinnett Jr G.W., Larsen WE: 'Wake vortex encounter hazard criteria for two aircraft classes'; NASA TM X-73,113, June 1976

Sammonds R.I., Stinnett Jr. G.W.: 'Hazard Criteria for Wake Vortex Encounters', NASA TM X-62.473, Moffet Field, CA, 1976

Go-Around Prediction during Landing

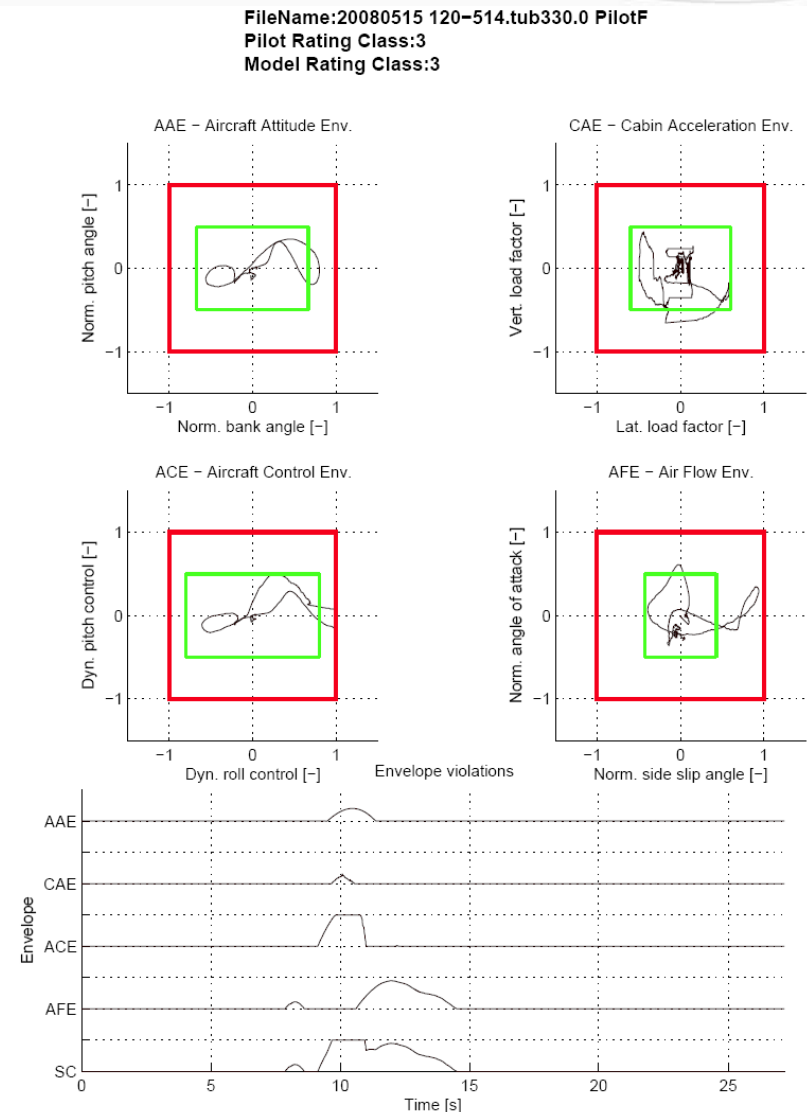


- 1623 WVEs
- 48 Session
- 40 Pilots
- 5 Aircraft
- 4 Simulators

➔ S-WAKE and NASA results in good agreement

Severity Criteria

- **Aircraft Attitude Envelope (AAE)**
 - Delta pitch angle
 - Bank angle
- **Cabin Acceleration Envelope (CAE)**
 - Vertical load factor
 - Lateral load factor
- **Aircraft Control Envelope (ACE)**
 - Sidestick pitch cmd
 - Sidestick roll cmd
- **Air Flow Envelope (AFE)**
 - Delta angle of attack
 - Sideslip angle



1. Is the performance of current **Pilot Models** (control behaviour and severity assessment) satisfying for WVE risk assessment?
2. Is there further research required? In which area?
2. How can validation and credibility of models be achieved